EGGLESTON DRAIN #0545

SECTION 17, T7N-R6E, FLINT TOWNSHIP, GENESEE COUNTY, MICHIGAN

PRELIMINARY ENGINEERING REPORT (PHASE I)

DECEMBER 2009

• PREPARED FOR •

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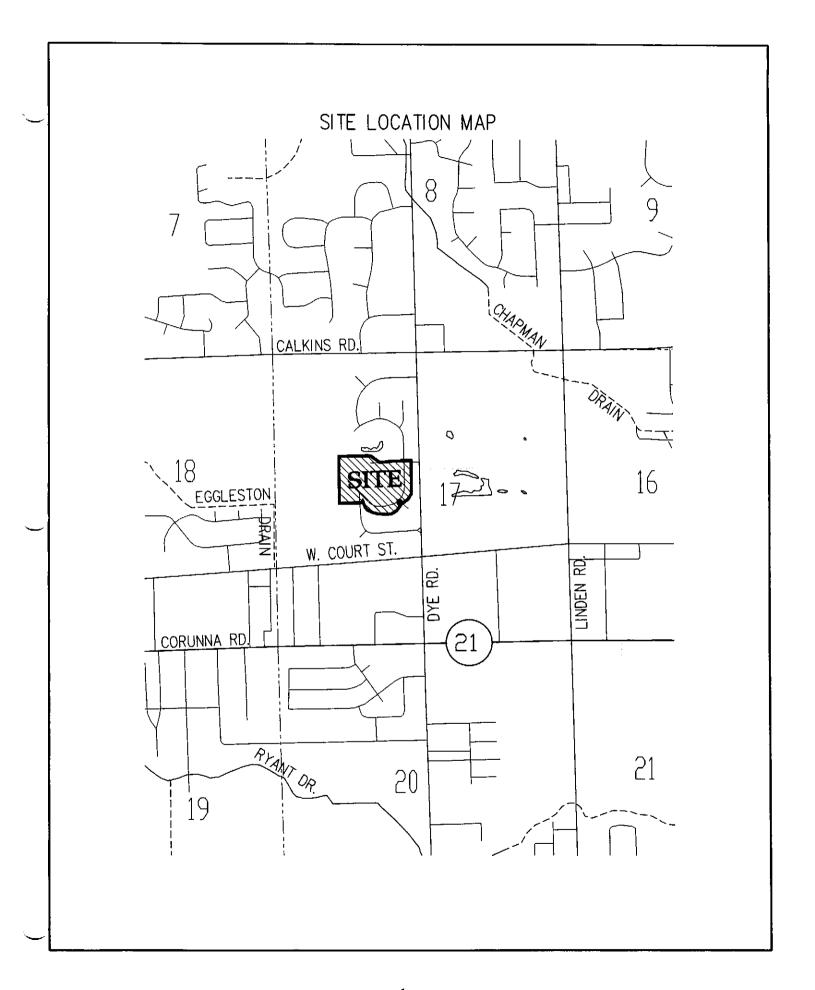
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° CIVIL ENGINEERS ° SURVEYORS ° LAND PLANNERS

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SUMMARY

The purpose of this report is to identify existing drainage concerns and issues, and to offer solutions for drainage problems occurring within the Eggleston Drain Drainage District. The study area is located north of Court Street and west of Dye Road in the southern half of the Dyewood Subdivisions and immediately to the west of the subdivision in Section 17 of Flint Township. The study area includes approximately twenty seven (27) acres of land, all tributary to the Eggleston Drain and all within the existing drainage district.¹

Presently there are drainage problems and concerns within the Dyewood Subdivision where existing residential properties are subject to flooding due to the lack of an adequate drainage system. Residents submitted a petition to the County Drain Commissioner of the County of Genesee, dated June 2, 2009. Various residents of the Dyewood Subdivision signed the petition calling for the cleaning, deepening, widening, straightening, extending, tiling, relocating, maintaining of the drain known and designated as the Eggleston Drain #0545.

A Board of Determination meeting was held at the Flint Township Hall on September 15, 2009. The recorded meeting minutes indicate that many of the residents had concerns about drainage problems and issues within the Dyewood Subdivisions. Residents expressed concerns over drainage improvements that will be necessary to facilitate the proposed Dyewood Subdivision road pavement rehabilitation project that is currently being designed by Kraft Engineering and Surveying, Inc. as a consultant to the Genesee County Road Commission. Following the petition and public comments, the Board of Determination determined that the Eggleston Drain project was necessary.

The existing drainage system for the study area consists of a combination of open ditch and storm sewer pipe. The downstream end of the existing main line drain system begins at the existing Eggleston Drain approximately 1,300 feet West of the Northwest corner of Lot 58 of Dyewood No. 4 Subdivision. An open ditch then proceeds Easterly 1,000 feet to the end of a 27 inch storm sewer. The existing 27 inch storm sewer then proceeds Easterly 300 feet, and Northeasterly 491 feet across South Dyewood Drive to the Northeasterly corner of Lot 61 of said Dyewood No. 4. A 12 inch storm sewer then proceeds Easterly 629 feet across the Islamic Center property to the Southeasterly corner of Lot 96 of Dyewood No. 5 Subdivision and point of ending. There is also a total of 603 feet of 12 inch storm sewer branches running along South Dyewood Drive to each side of the 27 inch storm sewer crossing this road.

We have determined from the meeting minutes, and from our direct observation of the study area that there are two main drainage issues relating to drainage concerns in this study area. The main issues to be addressed by this study therefore are as follows:

 The existing storm sewer outlet system outside of the public road right-of-way within Dyewood Subdivision is not currently a public county drain; it does not have continuous easement right-of-way; and the size, capacity, and structural condition of all of the existing storm sewer are of concern.

¹ See Page 1 "Site Location Map"

2. The existing open ditch outlet west of the Dyewood Subdivision running Westerly to the existing Eggleston Drain needs some cleanout and maintenance work, and it does not have any easement right-of-way.

From our observations, the existing storm sewer pipe in the subdivision does not exhibit any obvious visible major problems and it appears to be in reasonable working order. The existing open ditch west of the subdivision has sediment accumulation in the bottom, it is overgrown with brush and trees, and it needs some maintenance work. The Eggleston Drain itself is also overgrown and in need of maintenance.

POTENTIAL SOLUTIONS

Four alternative plans were developed to address drainage issues in the study area. Each plan would provide a drainage system that would provide a drainage outlet for the study area. The existing and/or proposed drainage system would collect drainage from all roads, yards, fields, and other areas within the study drainage area. The four alternative plans are described in detail later in this report.

DRAINAGE AREAS

For hydrologic analysis and preliminary design, a drainage area map was prepared showing the tributary areas.² The map is based upon aerial photogrammetry from the Genesee County Drain Commission, ca. 2002, current tax parcel and zoning information from Genesee County Equalization, existing as-built drawings of public record, satellite imagery from the National Map, 3/27/1999, and current survey data by Kraft Engineering & Surveying, Inc.

The drainage basin, and sub-basin areas were delineated on the Drainage Area Map. From the map, it has been determined that a total of 27 acres will be served by the proposed enclosed drainage system in the #0545 Eggleston Drain area. Additional area west of the Dyewood Subdivision area will drain directly to the open ditch between the Eggleston Drain and the Dyewood Subdivision area.²

² See Exhibit Nos. 9 – 12 "Drainage Maps"

LAND USE:

The existing land use within the drainage area consists of single family residential homes and vacant land. Parts of Dyewood No. 4 and Dyewood No. 5 Subdivisions are included within the study drainage area, along with the Southerly side of the Islamic property lying between North Dyewood Drive and South Dyewood Drive.

SOIL TYPES

Soil types have been determined from the "Soil Survey of Genesee County, Michigan", Map Sheet #24, April 1972, USDA. The predominant soil classification in this area is Perrin Loamy Sand and Boyer Loamy Sand.

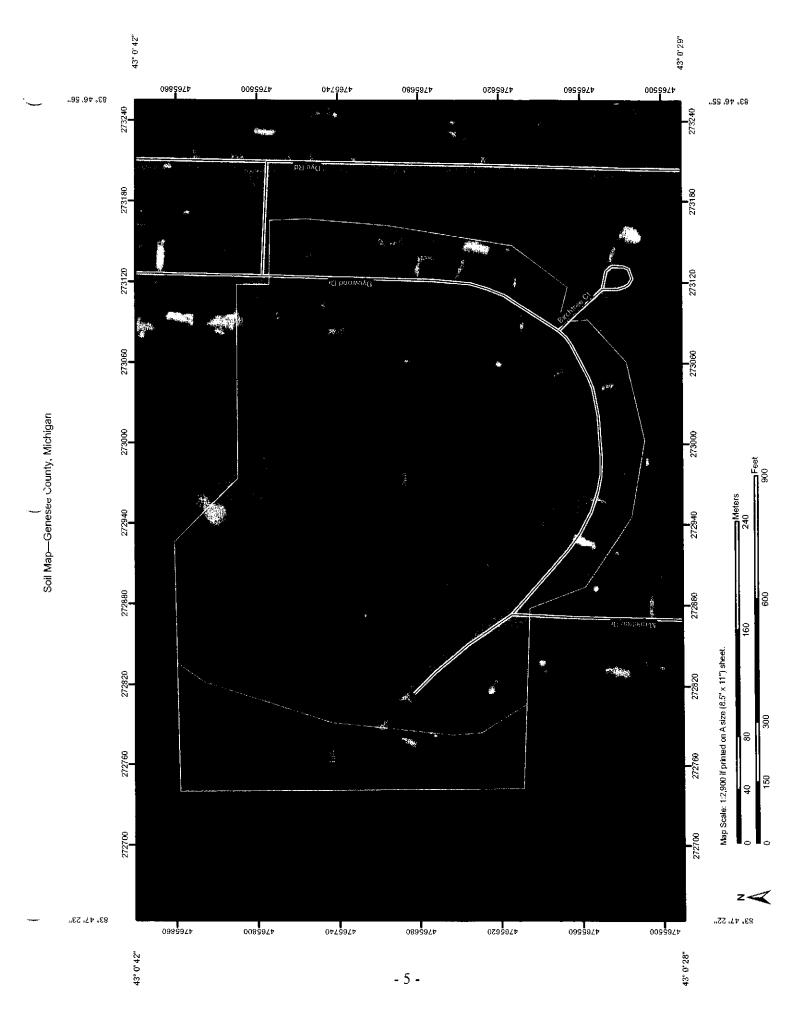
The hydrologic soil groups for the above soils, as defined by the Soil Conservation services, are as follows:

Map Unit Legend

	Genesee County, Michigan (MI049)												
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI										
BrA	Boyer loamy sand, 0 to 2 percent slopes	3.6	12.8%										
PeA	Perrin loamy sand, 0 to 2 percent slopes	24.5	87.2%										
Totals for	Area of Interest	28.1	100.0%										

PeA: The Perrin series consists of moderately well drained, nearly level and gently sloping sandy and loamy soils on washout plains and river terraces.

BrA: The Boyer series consists of well drained, nearly level to moderately steep soils that formed in sandy and loamy deposits.



HYDROLOGY

For this report, and for purposes of estimating pipe sizes and costs, the Rational Method has been used to determine peak runoff at various points of concentration in this watershed.

Use of the rational method is approved by the Genesee County Drain Commission for determining the 10-year flood flows for areas less than 300 acres in size. The standard form of the rational formula is:

Qp = C * i * A | where Qp is the peak flow in cubic feet per second, 'C' is a coefficient of runoff determined by surface conditions, 'i' is the rainfall intensity in inches/hour, and 'A' is the watershed area in acres.

In the Rational Method, many factors such as: land usage, land form, impervious surface area, rainfall, soils, slopes and conveyances are taken into account in the determination of the three factors.

The value for C is generally determined either by weighted averaging for the area under consideration, or by Engineer's estimation and judgment, or by consulting the Genesee County Drain Commission's regulatory chart based upon standard land usage patterns. For this report, the Genesee County Drain Commission's regulatory chart based upon standard land usage patterns was used to determine 'C'.

The rainfall intensity "i" may be determined from tabulated values, or from I.D.F. (Intensity, Duration, Frequency) charts for Genesee County, or from the formula:

i (10-yr) = 166.37 / (tc + 23.305) where 'tc' is the time of concentration in minutes for the drainage basin in question. For this report, the formula method was used.

Areas for 'A' were determined from the drainage area map.

ESTIMATED PEAK FLOWS

The mapped drainage areas were analyzed and peak flows determined using the Rational Method. A runoff coefficient of 0.25 was used for the large vacant grass/field/wooded areas, and a runoff coefficient of 0.35 was used for the subdivision residential lots along South Dyewood Drive.

To determine the rainfall intensity, the following information was used:

- Flow lengths were determined from the drainage area maps. The overall slope of the tributary area in the South Dyewood Drive area is flat.
- The types of cover in the drainage district were generally determined to be 'Grass Fields, Lawns, and Roadways.'
- Time of Concentration for sheet and waterway flows was determined using engineering judgement and the formula approved by the Genesee County Drain Commission.
- A minimum initial time of concentration of 30 minutes was selected. Pipeline transmission times were added to that to determine the downstream time of concentrations.
- The Genesee County Drain Commission's previously mentioned formula was then used to calculate the rainfall intensity for each drainage area.

Ten year flood flows were calculated for each map point, 1 thru 13, utilizing the overall drainage maps which can be found in Exhibits 5 thru 8 at the back of this report. The estimated ten year flood flows are summarized as follows:

#0545 EGGLESTON DRAIN IMPROVEMENTS

Location/Point		Estima	ated Peak	Flows (cfs	s)
<u>No.</u>	<u>Description</u>	Alt. No. 1	<u> Alt. No. 2</u>	Alt. No. 3	Alt No. 4
Pt. 1-2	Inlet	2.33	2.33	2.33	2.33
Pt. 2-4	Storm Sewer	}		4.11	4.11
Pt. 2-7	Storm Sewer	4.11	4.11		
Pt. 4-5	Storm Sewer				4.95
Pt. 4-9	Storm Sewer			5.49	
Pt. 5B-5	Storm Sewer	2.27	2.27	2.27	1.73
Pt. 5-10	Storm Sewer	4.19	4.19	4.79	7.70
Pt. 7-8	Storm Sewer	8.71	8.79	3.39	4.87
Pt. 8-9	Storm Sewer			9.19	
Pt. 8-10	Storm Sewer	14.41	14.41		10.66
Pt. 9-10	Storm Sewer			19.06	
Pt. 10-12	Storm Sewer	18.68	18.68	18.79	17.62
Pt. 11A-11	Storm Sewer	1.97	1.97	1.97	1.97
Pt. 11-12	Storm Sewer	4.09	4.09	4.09	4.09
Pt. 12-13	Storm Sewer	25.81	25.82	26.06	25.21
Pt. 13-Outlet	Storm Sewer	26.42	26.51	26.75	25.88

HYDRAULICS

To estimate both pipe, and channel sizes for this report, Genesee County Drain Commission standard calculations have been used.³

Hydraulic computations for both open channel flow and for enclosed pipe flow have been computed using "Manning's Equation", with standard Manning's friction coefficients specified by the Genesee County Drain Commission.

Manning's Equation derives from the empirical Chezy-Manning relationship used to study the relationship of channel velocity to parameters slope, channel bed condition, and shape. Its general form is:

 $V = 1.486 * R^{(2/3)} * S0^{(1/2)} / n - |$ where 'V' is average velocity, 'S0' is the slope, 'n' is the Manning's friction coefficient, 1.486 is a conversion factor to English Customary units, and 'R' is the hydraulic radius of the conveyance, determined from its geometry using the equation:

R = A/P | where 'A' is the cross-sectional area of flow, and 'P' is the wetted perimeter.

By substitution of V (average velocity) = Q (discharge) / A (area of cross-section), the equation may be solved for Q and placed in its common form (U.S. customary units) as:

 $Q = 1.486 * A * R^{(2/3)} * S0^{(1/2)} / n$

Values for 'n' were chosen from the GCDC-SWM's tabulated values.

³ See Exhibit Nos. 5 - 8, Storm Sewer System Design (spreadsheets)

ALTERNATIVES, DISCUSSION AND ESTIMATED COSTS

There are four alternatives that have been developed to establish and provide a drainage system to provide for the study area. All four alternatives would include improvements to the existing open ditch west of Dyewood No. 4 Subdivision, and east of the existing Eggleston Drain. Currently this existing open ditch is overgrown with trees and brush, and the ditch bottom is filled with sediment (approximately 1.7 feet of sediment depth at the end of the existing 27 inch storm sewer). The Genesee County Drain Commissioner — Division of Surface Water Management (GCDC-SWM) could maintain this open ditch once an easement has been obtained.

Alternatives Nos. 1 thru 4 are discussed as follows:

Alternative No. 1: See Exhibit No. 9 for a map of this alternative. This alternative would maintain the existing drainage system, except the existing storm sewer branches along South Dyewood Drive would be replaced.

The existing main line 27 inch and 12 inch storm sewer would remain in place as it currently exists, at least for the time being. Although sections of the existing main line storm sewer do not meet current standards, there are no obvious visible major problems with the existing sewer, the residents have not reported any known flooding issues, and it appears to be in reasonable working order. The existing sewer should be televised to make sure there are no internal structural problems if it is left in place. The main line storm sewer could be upgraded at a later time under a new petition if deemed necessary. The capacity of the existing main line sewer could be improved after the open ditch outlet has been cleaned out.

There are existing 12 foot wide platted drainage easements within the subdivision along the platted lot lines. These easements may need to be upgraded as determined by the GCDC - SWM. There is not any known existing easements along the 12 inch storm sewer crossing the Islamic Center property. New easement(s) for this section of sewer would need to be obtained

The existing 12 inch storm sewer branches along South Dyewood Drive would be replaced with new 15 inch storm sewer as part of the proposed Road Rehabilitation project for the Dyewood Subdivision that is currently in the design stage.

The estimated cost of Alternative No. 1, not including the cost of land or right-ofway, is as follows:

Alternative No. 1

Estimated Net Construction Cost = \$41,998.00
 Estimated Total Engineering Cost = \$11,339.00

Estimated Total Project Cost = \$53,337.00

See Exhibit No. 1 for detailed Cost Estimate for Alternative No. 1.

ALTERNATIVES, DISCUSSION AND ESTIMATED COSTS CONTINUED

Alternative No. 2: See Exhibit No. 10 for a map of this alternative. This alternative would rebuild the existing storm sewer system at its current location.

The existing 27 inch and 12 inch main line storm sewer would be replaced at its current location with a new larger storm sewer to meet current design standards. The existing 12 inch storm sewer branches along South Dyewood Drive would be replaced with new 15 inch storm sewer as part of the proposed Road Rehabilitation project for the Dyewood Subdivision that is currently in the design stage.

Easements would have to be obtained as noted under Alternative No. 1.

The estimated cost of Alternative No. 2, not including the cost of land or right-of-way, is as follows:

Alternative No. 2

1. Estimated Net Construction Cost = \$149,914.00 2. Estimated Total Engineering Cost = \$40,477.00

Estimated Total Project Cost = \$190,391.00

See Exhibit No. 2 for detailed Cost Estimate for Alternative No. 2.

Alternative No. 3: See Exhibit No. 11 for a map of this alternative. This alternative would rebuild the existing main line 27" storm sewer at its current location, and the existing main line 12" storm sewer crossing the Islamic Center property would be relocated along the rear lot lines adjacent to the Islamic Center property.

The existing 27 inch main line storm sewer would be replaced at its current location with a new larger storm sewer to meet current design standards. The existing 12 inch main line storm sewer across the Islamic Center property would be relocated across the rear lot lines of Lots 62 thru 64 of Dyewood No. 4 and Lots 97 thru 101 of Dyewood No. 5, and its size would be increased with a new larger storm sewer to meet current design standards. The existing 12 inch storm sewer branches along South Dyewood Drive would be replaced with new 15 inch storm sewer as part of the proposed Road Rehabilitation project for the Dyewood Subdivision that is currently in the design stage.

The existing 12 foot wide platted drainage easements within the subdivisions may have to be upgraded as determined as determined by the GCDC- SWM. Eight new easements would be required along the rear lot lines of said Lots 62 thru 64 and Lots 97 thru 101. This alternative would not require an easement from the Islamic Center property.

The estimated cost of Alternative No. 3, not including the cost of land or right-of-way, is as follows:

Alternative No. 3

1. Estimated Net Construction Cost = \$155,892.00 2. Estimated Total Engineering Cost = \$42,091.00

Estimated Total Project Cost = \$197,983.00

See Exhibit No. 3 for detailed Cost Estimate for Alternative No. 3.

ALTERNATIVES, DISCUSSION AND ESTIMATED COSTS CONTINUED

Alternative No. 4: See Exhibit No. 12 for a map of this alternative. This alternative would rebuild the existing main line 27" storm sewer at its current location Southwesterly of South Dyewood Drive, and the existing main line 12" storm sewer crossing the Islamic Center property would be relocated along South Dyewood Drive.

The existing 27 inch main line storm sewer would be replaced at its current location Southwesterly of South Dyewood Drive with a new larger storm sewer to meet current design standards. The existing 12 inch main line storm sewer crossing the Islamic Center property would be relocated to the right-of-way of South Dyewood Drive between Lot 62 of Dyewood No. 4 and Lot 97 of Dyewood No 5, and its size would be increased with a new larger storm sewer to meet current design standards. The existing 12" storm sewer branch on South Dyewood Drive Northwesterly of Lot 58 of Dyewood No. 4 would be replaced with a new 15" storm sewer as part of the proposed road rehabilitation project for the Dyewood Subdivision that is currently in the design stage.

The existing platted easements Southwesterly of South Dyewood Drive may have to be upgraded as determined by the GCDC - SWM. Some new easements may be required along the road in order to fit the new storm sewer along the road curve. This alternative would not require an easement from the Islamic Center property.

The estimated cost of Alternative No. 4, not including the cost of land or right-ofway is as follows:

Alternative No. 4

Estimated Net Construction Cost = \$164,593.00
 Estimated Total Engineering Cost = \$44,440.00

Estimated Total Project Cost = \$209,033.00

See Exhibit No. 4 for detailed Cost Estimate for Alternative No. 4.

RECOMMENDATIONS:

The recommended solution to properly address all drainage problems and concerns, and to meet current design standards to provide the required drainage capacity for the study area is to construct Alternative No. 2. Alternative No. 2 would upgrade the entire existing drainage system at its current location and along its existing established route in the most cost effective and practical manner.

Alternative No. 1 is not recommended because the size of the existing storm sewer does not meet current design standards and the exact structural condition of the existing pipe and drainage structures is unknown, and is of concern. The existing main line 27 inch and 12 inch storm sewer is in reasonable working order and could be utilized until a County Drain project is ready to be constructed. The residents have not reported any known flooding issues related to this existing storm sewer system.

Alternative Nos. 3 and 4 are both more costly than Alternative No. 2. Alternative Nos. 3 and 4 could be considered if easement acquisition becomes an issue that cannot be solved.

EXHIBIT NO. 1

ITEM	AMOUNT	UNIT		UNIT	٦	OTAL
			co	ST		
Driveway Removal and Replacement	100	SY	\$	30.00	\$	3,000
15" Sewer, Class III, Trench Detail 1	200	LF	\$	35.00	\$	7,000
15" Sewer, Class III, Trench Detail 2	403	ĹF	\$	40.00	\$	16,120
4 ft. diam. Drainage Structure, Catch Basin, 0 to 8 Ft.	3	EA	\$	1,200.00	\$	3,600
Drainage Structure Covers	1200	LB	\$	1.50	\$	1,800
Topsoil Surface, 4"	2500	SY	\$	2.00	\$	5,000
Chemical Fertilizer Nutrient (240 Lbs/Acre)	120	LB	\$	3.00	\$	360
Class A Seeding (200 Lbs/Acre)	100	LB	\$	4.00	\$	400
Mulch (2 Tons/Acre)	1	TON	\$	400.00	\$	400
Soil Erosion & Sedimentation Control Measures	1	LSUM	\$	500.00	\$	500
			Т		1	
Subtotal			\vdash		\$	38,180

Subtotal	\$	38,180
Contingency @ 10 percent	\$	3,818
Estimated Net Construction Costs	\$	41,998
Estimated Preliminary and Final Engineering Design	\$	5,040
Estimated Construction Engineering	\$	6,300
Engineering Total	\$	11,339
Total Estimated Project Cost (not including Land or Right-of-Way)	\$	53,337

ITEM	AMOUNT	UNIT		UNIT	-	ΓΟΤΑL
			CC	ST		
Road Surface Removal and Replacement	75	SY	\$	50.00	\$	3,750
Driveway Removal and Replacement	100	SY	\$	30.00	\$	3,000
Clearing and Grubbing	0.25	ACRE	\$	15,000.00	\$	3,750
15" Sewer, Class III, Trench Detail 1	200	LF	\$	35.00	\$	7,000
18" Sewer, Class III, Trench Detail 1	629	LF	\$	40.00	\$	25,160
30" Sewer, Class III, Trench Detail 1	214	ĹF	\$	55.00	\$	11,770
36" Sewer, Class III, Trench Detail 1	504	ĻF	\$	65.00	\$	32,760
15" Sewer, Class III, Trench Detail 2	403	LF	\$	40.00	\$	16,120
30" Sewer, Class III, Trench Detail 2	73	LF	\$	60.00	\$	4,380
4 ft. diam. Drainage Structure, Catch Basin, 0 to 8 Ft.	2	EA	\$	1,200.00	\$	2,400
5 ft. diam. Drainage Structure, Catch Basin, 0 to 8 Ft.	4	EA	\$	2,000.00	\$	8,000
Drainage Structure Covers	1650	LB	\$	1.50	\$	2,475
Steel End Pipe Section for 36" Concrete Pipe with Steel Bar Grate	1	EA	\$	1,200.00	\$	1,200
Plain Riprap	30	SY	\$	40.00	\$	1,200
Topsoil Surface, 4"	5000	SY	\$	2.00	\$	10,000
Chemical Fertilizer Nutrient (240 Lbs/Acre)	240	LB	\$	3.00	\$	720
Class A Seeding (200 Lbs/Acre)	200	LB	\$	4.00	\$	800
Mulch (2 Tons/Acre)	2	TON	\$	400.00	\$	800
Soil Erosion & Sedimentation Control Measures	1	LSUM	\$	1,000.00	\$	1,000
	1		1			
Subtotal			T		\$	136,285
Contingency @ 10 percent					\$	13,629
Estimated Net Construction Costs					\$	149,914
Estimated Preliminary and Final Engineering Design	-		╀		\$	17,990
Estimated Construction Engineering		-	╁		\$	********
Engineering Total	+	 	\vdash			22,487
Engineering Total	-		+		\$	40,477
Total Estimated Project Cost (not including Land or Right-of-Way)					\$	190,391

ITEM	AMOUNT	UNIT	Г	UNIT		TOTAL
			CC	ST		
Road Surface Removal and Replacement	75	SY	\$	50.00	\$	3,750
Driveway Removal and Replacement	100	SY	\$	30.00	\$	3,000
Clearing and Grubbing	0.25	ACRE	\$	15,000.00	\$	3,750
15" Sewer, Class III, Trench Detail 1	200	LF	\$	35.00	\$	7,000
18" Sewer, Class III, Trench Detail 1	770	LF	\$	40.00	\$	30,800
30" Sewer, Class III, Trench Detail 1	194	LF	\$	55.00	\$	10,670
36" Sewer, Class III, Trench Detail 1	504	LF	\$	65.00	\$	32,760
15" Sewer, Class III, Trench Detail 2	403	LF	\$	40.00	\$	16,120
30" Sewer, Class III, Trench Detail 2	73	LF	\$	60.00	\$	4,380
4 ft. diam. Drainage Structure, Catch Basin, 0 to 8 Ft.	5	EA	\$	1,200.00	\$	6,000
5 ft. diam. Drainage Structure, Catch Basin, 0 to 8 Ft.	4	EA	\$	2,000.00	\$	8,000
Drainage Structure Covers	2700	LB	\$	1.50	\$	4,050
Steel Pipe End Section for 36" Concrete Pipe with Steel Bar Grate	1	EA	\$	1,200.00	\$	1,200
Topsoil Surface, 4"	3750	SY	\$	2.00	\$	7,500
Chemical Fertilizer Nutrient (240 Lbs/Acre)	180	LB	\$	3.00	\$	540
Class A Seeding (200 Lbs/Acre)	150	LB	\$	4.00	\$	600
Mulch (2 Tons/Acre)	1.5	TON	\$	400.00	\$	600
Soil Erosion & Sedimentation Control Measures	1	LSUM	\$	1,000.00	\$	1,000
					L.	
Subtotal					\$	141,720
Contingency @ 10 percent				_	\$	14,172
Estimated Net Construction Costs					\$	155,892
Estimated Preliminary and Final Engineering Design			\vdash		\$	18,707
Estimated Construction Engineering					\$	23,384
Engineering Total					\$	42,091
Total Estimated Project Cost (not including Land or Right-of-Way)			\vdash		\$	197,983

ITEM	AMOUNT	UNIT		UNIT	-	TOTAL
			CC	ST		
Road Surface Removal and Replacement	200	SY	\$	50.00	\$	10,000
Driveway Removal and Replacement	250	SY	\$	30.00	\$	7,500
Clearing and Grubbing	0.25	ACRE	\$	15,000.00	\$	3,750
15" Sewer, Class III, Trench Detail 1	200	LF	\$	35.00	\$	7,000
36" Sewer, Class III, Trench Detail 1	504	LF	\$	65.00	\$	32,760
15" Sewer, Class III, Trench Detail 2	54	LF	\$	40.00	\$	2,160
18" Sewer, Class III, Trench Detail 2	745	LF	\$	45.00	\$	33,525
21" Sewer, Class III, Trench Detail 2	349	LF	\$	50.00	\$	17,450
30" Sewer, Class III, Trench Detail 2	73	LF	\$	55.00	\$	4,015
4 ft. diam. Drainage Structure, Catch Basin, 0 to 8 Ft.	6	EA	\$	1,200.00	\$	7,200
5 ft. diam. Drainage Structure, Catch Basin, 0 to 8 Ft.	3	EΑ	\$	2,000.00	\$	6,000
Drainage Structure Covers	2500	LB	\$	1.50	\$	3,750
Steel Pipe End Section for 36" Concrete Pipe with Steel Bar Grate	1	EA	\$	1,200.00	\$	1,200
Topsoil Surface, 4"	5000	SY	\$	2.00	\$	10,000
Chemical Fertilizer Nutrient (240 Lbs/Acre)	240	LB	\$	3.00	\$	720
Class A Seeding (200 Lbs/Acre)	200	LB	\$	4.00	\$	800
Mulch (2 Tons/Acre)	2	TON	\$	400.00	\$	800
Soil Erosion & Sedimentation Control Measures	1	LSUM	\$	1,000.00	\$	1,000
			Π		<u> </u>	
Subtotal				<u></u>	\$	149,630
Contingency @ 10 percent					\$	14,963
Estimated Net Construction Costs			ļ		\$	164,593
Estimated Preliminary and Final Engineering Design					\$	19,751
Estimated Construction Engineering					\$	24,689
Engineering Total					\$	44,440
Total Estimated Project Cost (not including Land or Right-of-Way)	_				\$	209,033

DYE WOOD Tim O'Dell December 17, 2009

Job Name By Date

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		Existing Storm server	Existing Storm some	Livering Schieber	Existing Storm sewer to DS #10	Externa Server	Proposed Storm sever to DS #6	Proposed Storm sever to DS #10	Existing Storm server to DS #12	Existing Storm sewer	Proposed Storm sewer to DS #12	Existing Storm sewer	Existing Storm sewer to Open Drain
TIME OF FLOW	MIN.	90'0	3.19	09:0	0:30	0.15	0.79	0.91	0.31	0.07	1.17	0.84	1.24
VELOCITY OF	FT/SEC	7.22	2.46	4.45	3.96	2.69	3.42	3.42	3.96	5.98	3.61	4.05	4.05
SCOPE OF H.G.	%												
SLOPE OF PIPE	%	2.16	0.25	0.82	0.22	0:30	0.36	0.36	0.22	1.48	0.40	0.23	0.23
LENGTH OF PIPE TOURTS TXBN OT	H.	25	470	159	214	25	163	186	73	25	254	204	300
ABTEMAIG BAIG TO	Ż	12	12	12	27	12	15	15	27	12	15	27	27
FLOW G=1 TOTAL CA1	C.F.S.	2.33		8.7	1.3	2.27	6.19	(1)	1868	1.97	4 09	25.83	26.42
RAINFALL INTENSITY I	IN/HR	3.12	3.12	2.94	2.91	3.12	3.11	3.07	2.87	3.12	3.12	2.85	2.81
T 3MIT	MIN	30.00	30.06	33.25	33.85	30.00	30.15	30.95	34.75	30.00	30.07	35.06	36.00
YOTAL EQUIV.	٧	0.75	1.32	2.96	4.95	0.73	1.35	1.35	7.75	0.63	1.31	9.06	9.42
EQUIVALENT I A D A3RA		0.75	0.57	1.64	1.99	0.73	0.62	0.00	0.00	0.63	99.0	0.00	0.36
UNOFF COEF. C	8	0.35	0.35	0.25	0.25	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35
A A3AA	Ş.	2.13	3.77	10.34	18.29	2.08	3.85	3.85	22.14	1.80	3.75	25.89	26.91
INCREMENT IA AЭЯA	AC.	2.13	1.64	6.57	7.95	2.08	1.77	00:00	00:00	1.80	1.95	0:00	1.02
INCREMENT IA AЭЯA	SFI	92800	71450	286200	346300	00906	77100	0	0	78400	84950	0	44400
STRUCTURE #		-	2	7	8	58	32	9	10	11A	11	12	13

Job Name DYE WOOD By Tim O'Dell Date December 17, 2009				Existing Storm sewer	Proposed Storm sevier	Proposed Storm sewer	Proposed Storm sever to DS #10	Seven Work	Proposed Storm sower	Proposed Storm sever to DS #10	Proposed Storm sewer to DS #12	Edisting Storm server	5	Proposed Storm sewer	Proposed Storm sewer to Drain Outlet
166.37 + 23.31	WOJ = OF FLOW	MIN.		90:0	2.72	0.53	0.84	0.15	0.79	0.91	0.29	0.07	1.17	0.69	1.02
-	VELOCITY OF	FT/SEC		7.22	2.88	4.99	4.25	2.69	3.42	3.42	4.25	5.98	3.61	4.90	4.90
- 6	SLOPE OF H.G.	%													
	STOPE OF PIPE	%		2.16	0.20	09:0	0.22	0:30	0.36	0.36	0.22	1.48	0.40	0.23	0.23
	LENGTH OF PIPE. TOURTS TXBUCT.	Ħ.	·	25	470	159	214	25	163	186	73	25	254	204	300
T.	DIAMETER OF PIPE	ż		12	18	18	30	12	15	15	30	12	15	36	98
Q = CIA															
Ŭ	G=1 TOTAL CAI	C.F.S.		2.33	4:11	8.79	14.54	227	4.19	4.13	18.88	1.97	4.09	26.11	28.51
	I YTISNƏTNI I YTISNƏTNI	IN/HR		3.12	3.12	2.97	2.94	3.12	3.11	3.07	2.90	3.12	3.12	2.88	2.81
1/2	TIMET	MIN.		30.00	90.06	32.78	33.31	30.00	30.15	30.95	34.15	30.00	30.07	34.44	35.81
2/3 S	TOTAL EQUIV. REA TOTAL CAI	٧		0.75	1.32	2.96	4.95	0.73	1.35	1.35	7.75	0.63	1.31	9.06	9.42
ď	TNALENT I A D ABRA			0.75	0.57	1.64	1.99	0.73	0.62	0.00	0.00	0.63	0.68	0.00	0.36
88	UNOFF COEF. C	ľ		0.35	0.35	0.25	0.25	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35
1.486 n	TOTAL A A39A	AC.		2.13	3.77	10.34	18.29	2.08	3.85	3.85	22.14	1.80	3.75	25.89	26.91
∀ ⊌	TNEMENTI IA ABRA	AC.		2.13	164	6.57	7.95	2.08	1.77	0.00	0.00	1.80	1.95	0.00	1.02
	INCREMENT AREA Ai	SFT		92800	71450	286200	346300	00906	77100	0	0	78400	84950	0	44400
	STRUCTURE #			~	2	7	8	2B	S	9	10	11A	=	12	13

DYE WOOD Tim O'Dell December 1, 2009

Job Name By Date

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				•	· :.	4	•										.)	Suffer
		Existing Storm sewer	Proposed Storm sewer	Existing Storm sewer	Proposed Storm sewer	Proposed Storm sewer	Existing Storm sewer	Existing Storm sawer	Proposed Storm sewer	Proposed Storm sewer	Existing Storm sower	Proposed Storm sewer	Proposed Storm sewer	Proposed Storm sewer to Outlet Drain				
WOJ = OF FLOW	MIN.	90.0	1.07	0.75	0.75	0.72	0.87	0.15	0.79	0.91	09.0	0.08	0.76	0.29	0.07	1.17	0.69	1.02
VELOCITY OF	FT/SEC	7.22	2.88	2.88	2.88	3.22	3.53	2.69	3.42	3.42	4.45	3.96	4.25	4.25	5.98	3.61	4.90	4.90
SLOPE OF H.G.	%																	
SLOPE OF PIPE	%	2.16	0.20	0.20	0.20	0.25	0:30	0:30	0.36	0.36	0.82	0.22	0.22	0.22	1.48	0.40	0.23	0.23
LENGTH OF PIPE TO NEXT STRUCT.	FT.	25	185	130	130	140	185	25	163	186	159	20	194	73	25	254	204	300
PIAMETER 3919 70	Z.	12	18	18	18	18	18	12	15	15	12	27	30	30	12	15	36	36
G = 1 101AL C.A.I	C.F.S.	2.83		4.57	5.03	5.49	6039	2.27	4.19		3.39	9.19	19.06	18.81	1.97	4.09	26.06	28.75
RAINFALL INTENSITY I	IN/HR	3.12	3.12	3.06	3.01	2.97	3.01	3.12	3.11	3.07	2.97	2.94	2.93	2.89	3.12	3.12	2.88	2.84
T AMIT	M.	30.00	30.06	31.13	31.88	32.63	31.88	30.00	30.15	30.95	32.75	33.35	33.43	34.19	30.00	30.07	34.53	35.27
TOTAL EQUIV.	₽¥	0.75	1.32	1.49	1.67	1.85	2.02	0.73	1.35	1.35	1.14	3.13	6.50	6.50	0.63	1.31	9.06	9.42
EQUIVALENT		0.75	0.57	0.18	0.18	0.18	0.18	0.73	0.62	0.00	1.14	1.99	00:0	0.00	0.63	0.68	0.00	0.36
NOPE COEF. C	Я	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.25	0.25	0.35	0.35	0.35	0.35	0.35	0.35
JATOT A A∃ЯA	¥C.	2.13	3.77	4.27	4.77	5.27	5.77	2.08	3.85	3.85	4.57	12.52	0.00	0.00	1.80	3.75	25.89	26.91
INCREMENT IA ABRA	AC.	2.13	1.64	0.50	0.50	0.50	0.50	2.08	1.77	0.00	4.57	7.95	00.0	0.00	1.80	1.95	0.00	1.02
INCREMENT IA ABRA	SFT	92800	71450	21800	21800	21800	21800	00906	77100	0	199100	346300	0	0	78400	84950	0	44400
# ЗЯПТОПЯТЕ		-	2	3	3A	4	44	58	9	9	2	80	6	10	11A	1	12	13

Job Name DYE WOOD By Tim O'Dell Date December 1, 2009				Elisting Storm sewer	Proposed Storm sewer	Proposed Storm sower	Proposed Storm sever	Casting Storm server	Proposed Stoff sewer	Proposed Storm sewer	Existing Sterm; sewer	Feeding Sever	Proposed Storm: sewer	Extering Storm sower	Processed Storm sower	Proposed Storm sewer	Proposed Storm sewer to Outlet Drain
166.37 + 23.31	WOJA 40 EMIT	MIN		90:0	1.16	1.59	1.56	0.15	0.85	0.97	09'0	06:0	0.29	0.07	1.17	69:0	1.02
 -	VELOCITY OF	FT/SEC		7.22	2.88	2.88	2.88	2.69	3.19	3.19	4.45	3.96	4.25	5.98	3.61	4.90	4.90
<u> </u>	SLOPE OF H.G.	%															
	STOPE OF PIPE	%		2.16	0.20	0.20	0.20	0:30	0.20	0.20	0.82	0.22	0.22	1.48	0.40	0.23	0.23
	LENGTH OF PIPE TO NEXT STRUCT.	Ξ.		52	200	275	270	25	163	186	159	214	73	25	254	204	300
	PIAMETER OF PIPE	<u>z</u>		12	18	18	18	12	21	21	12	27	30	12	15	36	9E
Q = CIA	INTENSITY	HR C.F.S.		12 238	12 41	0.5 4:03	96	12 173	88 7.70	7,59	97 4.87	10.88	30 17,62	1.97	12 4.09	78 25.21	75 25.88
	RAINFALL	Į.		3.12	3.12	22 3.05	.81 2.96	3.12	37 2.88	22 2.84	75 2.97	35 2.94	19 2.80	3.12	3.12	9 2.78	2.75
3 1/2 S	TOTAL EQUIV. REA TOTAL C B I	∀ N <u>M</u>		0.75 30.00	1.32 30.06	1.32 31.22	1.67 32.8	0.55 30.00	2.67 34.37	2.67 35.22	1.64 32.75	3.63 33.35	6.30 36.19	0.63 30.00	.31 30.07	9.06 36.49	9.42 37.23
23	I A D ABRA			0.75	0.57	0.00	0.35	0.55	0.44		1.64	86.	00.0	0.63	0.68	00.00	0.36
	UNOFF COEF. C	В	-	0.35	0.35	0.35	0.35 (0.35	0.35	0.35	0.25	0.25	0.35	0.35 0	0.35	0.35 0	0.35 0
1.486 n	JATOT A A3RA	AC.		2.13	3.77	3.77	4.77	1.58	7.62	7.62	6.57	14.52	22.14 (1.80	3.75	25.89	26.91
A = 0	INCREMENT IA A39A	ÅC.		2.13	2.	0.00	1.00	1.58	1.27	0.00	6.57	7.95	0.00	1.80	1.95	0.00	1.02
	INCREMENT IA ABRA	SFT		92800	71450	0	43560	00889	55300	0	286200	346300	0	78400	84950	0	44400
	# BAUTOURTS			-	2	က	4	98 8	ı,	9	2	8	10	11A	-	12	13

